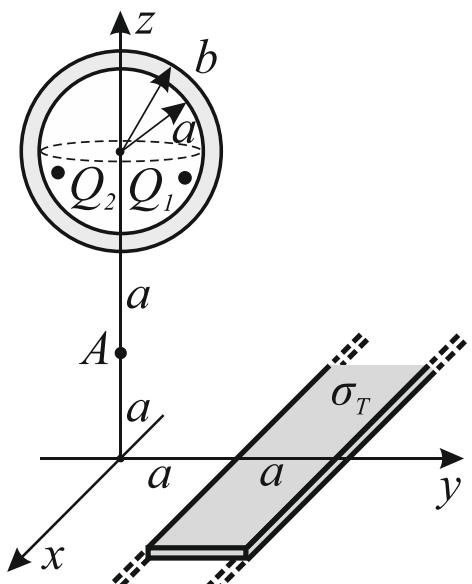


ZADACI

Zadatak 1. Nenaelektrisana provodna sferna ljeska, unutrašnjeg poluprečnika a i spoljašnjeg poluprečnika b , postavljena je kao što je prikazano na slici 1. Centar ljeske se nalazi na z osi, na udaljenosti $2a+b$ od centra Dekartovog koordinatnog sistema i unutar nje se nalaze dva tačkasta nenelektrisanja, Q_1 i Q_2 . Tanka, veoma dugačka, traka od dielektrika, širine a , ravnomerno je nenelektrisana površinskim nenelektrisanjem σ_T i postavljena u x - y ravni, paralelno sa x osom. Sferna ljeska i traka se nalaze na dovoljno velikom međusobnom rastojanju, tako da je njihov međusobni uticaj na raspodelu nenelektrisanja zanemarljiv. Sistem se nalazi u vazduhu.

- Odrediti, u opštim brojevima, ukupne količine nenelektrisanja na unutrašnjoj i spoljašnjoj površi provodne ljeske.
- Odrediti, u opštim brojevima, ukupni vektor jačine električnog polja koji u tački A stvaraju sferna ljeska i traka. Tačka A se nalazi na z osi, na visini a .
- Odrediti površinsko nenelektrisanje trake, σ_T , tako da ukupni vektor jačine električnog polja u tački A nema z komponentu.

Brojni podaci su: $a = 1 \text{ cm}$, $b = 1,1 \text{ cm}$, $Q_1 = 2 \text{ nC}$, $Q_2 = 5 \text{ nC}$, $\epsilon_0 = 8,85 \cdot 10^{-12} \text{ F/m}$.



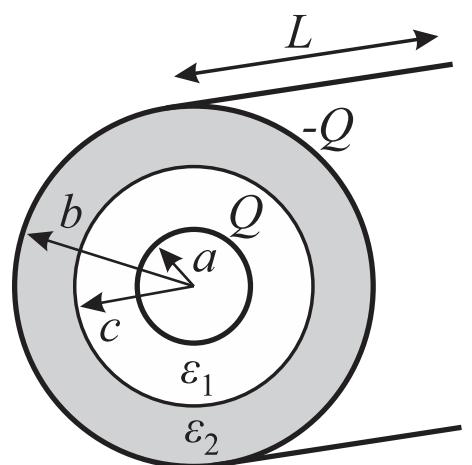
Slika 1.

$$\int \operatorname{tg} \alpha d\alpha = -\ln |\cos \alpha|$$

Zadatak 2. Na slici 2 je prikazan koaksijalni kabl dužine $L = 1 \text{ m}$, ispunjen sa dva sloja dielektrika: čvrsti – relativne permitivnosti $\epsilon_{r1} = 5$ i tečni – relativne permitivnosti ϵ_{r2} . Poluprečnici elektroda kabla su a i b , dok je poluprečnik razdvojne površi dva dielektrika c .

- Odrediti poluprečnik razdvojne površi dva dielektrika, c , ako je najveći intenzitet vektora jačine električnog polja u čvrstom dielektriku, permitivnosti ϵ_1 , duplo veći od najmanjeg intenziteta vektora jačine električnog polja u tom sloju.
- Odrediti relativnu permitivnost tečnog dielektrika, ϵ_{r2} , ako se nakon njegovog potpunog ispuštanja iz kabla, ukupna količina vezanog nenelektrisanja uz razdvojnu površ dva dielektrika poveća četiri puta.
- Odrediti, u opštim brojevima, izraz za kapacitivnost kondenzatora, pre ispuštanja tečnog dielektrika.

Ostali brojni podaci: $a = 1 \text{ cm}$, $b = 5 \text{ cm}$, $Q = 1 \text{ nC}$.



Slika 2.

PRAVILA POLAGANJA

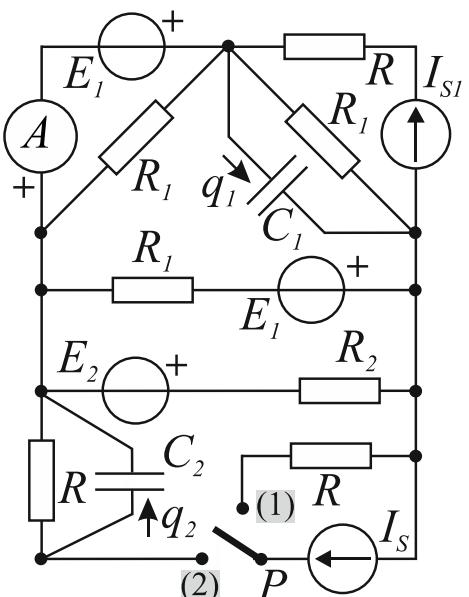
Za položen kolokvijum neophodno je sakupiti više od 50% poena na svakom od zadataka. Svaki zadatak se boduje sa 25 poena. Kolokvijum traje jedan sat i trideset minuta.

ZADACI

Zadatak 1. Kada se u kolu vremenski konstantnih struja sa slike 1 preklopnik prebaci iz položaja (1) u položaj (2), kroz kondenzator kapacitivnosti $C_1 = 4 \text{ nF}$ protekne količina nanelektrisanja $q_1 = 6 \text{ nC}$, u naznačenom referentnom smeru.

- Primenjujući teoremu superpozicije, odrediti jačinu struje strujnog generatora, I_S , kao i količinu nanelektrisanja q_2 , koja protekne kroz kondenzator kapacitivnosti $C_2 = 1 \text{ nF}$, u naznačenom referentnom smeru, nakon prebacivanja preklopnika iz položaja (1) u položaj (2).
- Izračunati snagu strujnog generatora I_{S1} u stacionarnom stanju mreže, koje nastane kada je preklopnik u položaju (2). Kolo rešavati primenom metode potencijala čvorova.
- Izračunati pokazivanje idealnog ampermetra, kada je preklopnik u položaju (2).

Brojni podaci su: $E_1 = 3 \text{ V}$, $E_2 = 5 \text{ V}$, $I_{S1} = 0,5 \text{ A}$, $R_1 = 5 \Omega$, $R_2 = 10 \Omega$, $R = 20 \Omega$.

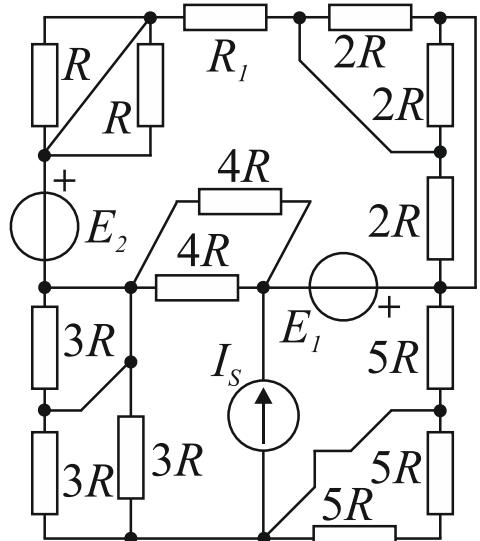


Slika 1.

Zadatak 2. U kolu vremenski konstantnih struja, sa slike 2, otpornost otpornika R_1 je takva da se na njemu razvija maksimalno moguća snaga.

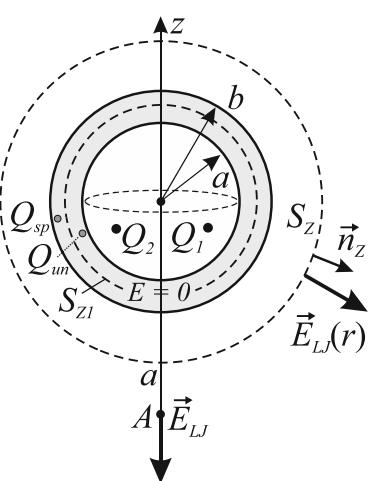
- Nacrtati pojednostavljenu šemu kola, zamenom grupa otpornika otpornosti R , $2R$, $3R$, $4R$ i $5R$ sa po jednim otpornikom.
- Primenom Tevenenove teoreme, izračunati vrednost otpornosti otpornika R_1 .
- Primenom metode konturnih struja, izračunati snage svih generatora u kolu.

Brojni podaci su: $R = 51 \Omega$, $E_1 = E_2 = 51 \text{ V}$, $I_S = 1 \text{ A}$.



I-1

a)



$$\oint_{S_{Z1}} \vec{E} \cdot d\vec{S} = \frac{Q_{unutar S_{Z1}}}{\epsilon_0} \quad E = 0, \text{ u provodniku}$$

$$0 = \frac{(Q_1 + Q_2) + Q_{un}}{\epsilon_0} \quad Q_{un} = -Q_1 - Q_2$$

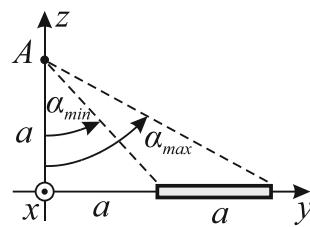
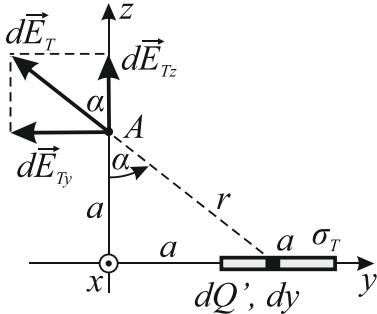
$$Q_{LJ} = Q_{un} + Q_{sp} = 0 \quad Q_{sp} = -Q_{un} = Q_1 + Q_2$$

b)

$$\oint_{S_z} \vec{E} \cdot d\vec{S} = \frac{Q_{unutar S_z}}{\epsilon_0} \quad \nabla(\vec{E}_{LJ}, \vec{n}_z) = 0$$

$$E_{LJ}(r) 4\pi r^2 = \frac{Q_1 + Q_2 + Q_{un} + Q_{sp}}{\epsilon_0} = \frac{Q_1 + Q_2}{\epsilon_0} \quad E_{LJ}(r) = \frac{Q_1 + Q_2}{4\pi\epsilon_0 r^2}, \quad r > b$$

$$E_{LJ} = E_{LJuA}(r = a + b) = \frac{Q_1 + Q_2}{4\pi\epsilon_0(a+b)^2} \quad \boxed{\vec{E}_{LJ} = \frac{Q_1 + Q_2}{4\pi\epsilon_0(a+b)^2} \cdot (-\vec{i}_z)}$$



$$dQ = \sigma_T dS = \sigma l dy \quad (l \rightarrow \infty)$$

$$\frac{dQ}{l} = \sigma_T dy$$

$$dQ' = \sigma_T dy$$

$$dE_{Ty} = dE_T \sin \alpha = \frac{dQ'}{2\pi\epsilon_0 r} \sin \alpha = \frac{\sigma_T dy}{2\pi\epsilon_0 r} \sin \alpha = \frac{\sigma_T \frac{r d\alpha}{\cos \alpha}}{2\pi\epsilon_0 r} \sin \alpha = \frac{\sigma_T}{2\pi\epsilon_0} \operatorname{tg} \alpha d\alpha$$

$$E_{Ty} = \int dE_{Ty} = \frac{\sigma_T}{2\pi\epsilon_0} \int_{\alpha_{min}}^{\alpha_{max}} \operatorname{tg} \alpha d\alpha = \frac{\sigma_T}{2\pi\epsilon_0} (-\ln |\cos \alpha|) \Big|_{\alpha_{min}}^{\alpha_{max}} = \frac{\sigma_T}{2\pi\epsilon_0} (\ln |\cos \alpha_{min}| - \ln |\cos \alpha_{max}|) = \frac{\sigma_T}{2\pi\epsilon_0} \ln \frac{|\cos \alpha_{min}|}{|\cos \alpha_{max}|}$$

$$E_{Ty} = \frac{\sigma_T}{2\pi\epsilon_0} \ln \frac{\frac{a}{\sqrt{a^2 + a^2}}}{\frac{a}{\sqrt{a^2 + (2a)^2}}} = \frac{\sigma_T}{2\pi\epsilon_0} \ln \frac{\sqrt{5}}{\sqrt{2}} \quad \boxed{\vec{E}_{Ty} = \frac{\sigma_T}{2\pi\epsilon_0} \ln \frac{\sqrt{5}}{\sqrt{2}} \cdot (-\vec{i}_y)}$$

$$dE_{Tz} = dE_T \cos \alpha = \frac{dQ'}{2\pi\epsilon_0 r} \cos \alpha = \frac{\sigma_T dy}{2\pi\epsilon_0 r} \cos \alpha = \frac{\sigma_T \frac{r d\alpha}{\cos \alpha}}{2\pi\epsilon_0 r} \cos \alpha = \frac{\sigma_T}{2\pi\epsilon_0} d\alpha$$

$$E_{Tz} = \int dE_{Tz} = \frac{\sigma_T}{2\pi\epsilon_0} \int_{\alpha_{min}}^{\alpha_{max}} d\alpha = \frac{\sigma_T}{2\pi\epsilon_0} (\alpha_{max} - \alpha_{min}) = \frac{\sigma_T}{2\pi\epsilon_0} \left(\operatorname{arctg} \frac{2a}{a} - \operatorname{arctg} \frac{a}{a} \right) \quad \boxed{\vec{E}_{Tz} = \frac{\sigma_T}{2\pi\epsilon_0} (\operatorname{arctg} 2 - \operatorname{arctg} 1) \cdot \vec{i}_z}$$

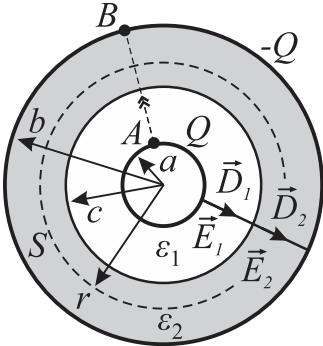
c)

$$\vec{E}_A = \vec{E}_{Ty} + \vec{E}_{Tz} + \vec{E}_{LJ} = \frac{\sigma_T}{2\pi\epsilon_0} \ln \frac{\sqrt{5}}{\sqrt{2}} \cdot (-\vec{i}_y) + \frac{\sigma_T}{2\pi\epsilon_0} (\operatorname{arctg} 2 - \operatorname{arctg} 1) \cdot \vec{i}_z + \frac{Q_1 + Q_2}{4\pi\epsilon_0 (a+b)^2} \cdot (-\vec{i}_z)$$

$$\vec{E}_{Az} = 0 \Rightarrow \frac{\sigma_T}{2\pi\epsilon_0} (\operatorname{arctg} 2 - \operatorname{arctg} 1) = \frac{Q_1 + Q_2}{4\pi\epsilon_0 (a+b)^2} \quad \boxed{\sigma_T = 24,7 \mu C / m^2}$$

I-2

a)



Granični uslov:

$$D_{n1} = D_{n2} \quad D_1 = D_2 = D$$

$$E_{t1} = E_{t2} = 0$$

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{slobodno u S}$$

$$\int_{S_{OM}} D ds = Q$$

$$D 2r\pi L = Q$$

$$D = \frac{Q}{2\pi r L}, \quad a \leq r \leq b$$

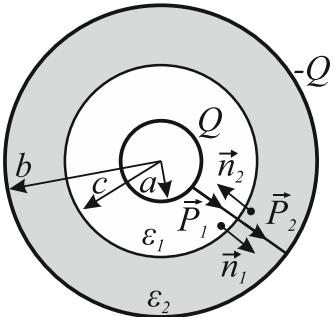
$$E_1 = \frac{D}{\epsilon_1} = \frac{Q}{2\pi\epsilon_1 r L}, \quad a \leq r \leq c$$

$$E_2 = \frac{D}{\epsilon_2} = \frac{Q}{2\pi\epsilon_2 r L}, \quad c \leq r \leq b$$

$$\left. \begin{aligned} E_{1\max}(r=a) &= \frac{Q}{2\pi\epsilon_1 a L} \\ E_{1\min}(r=c) &= \frac{Q}{2\pi\epsilon_1 c L} \end{aligned} \right\} \Rightarrow$$

$$E_{1\max} = 2 E_{1\min}, \quad \frac{Q}{2\pi\epsilon_1 a L} = 2 \cdot \frac{Q}{2\pi\epsilon_1 c L} \quad c = 2a \quad [c = 2 \text{ cm}]$$

b)



Pre ispuštanja ε2:

$$P = D - \epsilon_0 E = D - \epsilon_0 \frac{D}{\epsilon} = \left(1 - \frac{1}{\epsilon_r}\right) D = \left(1 - \frac{1}{\epsilon_r}\right) \frac{Q}{2\pi r L}$$

$$\sigma_{V1}^{PRE} = \vec{P}_1 \cdot \vec{n}_1 = P_1(c) = \left(1 - \frac{1}{5}\right) \frac{Q}{2\pi c L} = \frac{4}{5} \frac{Q}{2\pi c L}$$

$$\sigma_{V2}^{PRE} = \vec{P}_2 \cdot \vec{n}_2 = -P_2(c) = -\left(1 - \frac{1}{\epsilon_{r2}}\right) \frac{Q}{2\pi c L}$$

$$Q_V^{PRE} = (\sigma_{V1}^{PRE} + \sigma_{V2}^{PRE}) 2\pi c L \quad Q_V^{PRE} = \left[\frac{4}{5} - \left(1 - \frac{1}{\epsilon_{r2}}\right) \right] Q$$

Posle ispuštanja ε2:

$$\sigma_{V1}^{POSLE} = \sigma_{V1}^{PRE} = \vec{P}_1 \cdot \vec{n}_1 = P_1(c) = \left(1 - \frac{1}{5}\right) \frac{Q}{2\pi c L} = \frac{4}{5} \frac{Q}{2\pi c L} \quad \sigma_{V2}^{POSLE} = 0$$

$$Q_V^{POSLE} = \sigma_{V1}^{POSLE} 2\pi c L \quad Q_V^{POSLE} = \frac{4}{5} Q$$

$$Q_V^{POSLE} = 4Q_V^{PRE}, \quad \frac{4}{5} Q = 4 \cdot \left[\frac{4}{5} - \left(1 - \frac{1}{\epsilon_{r2}}\right) \right] Q \quad \epsilon_{r2} = 2,5$$

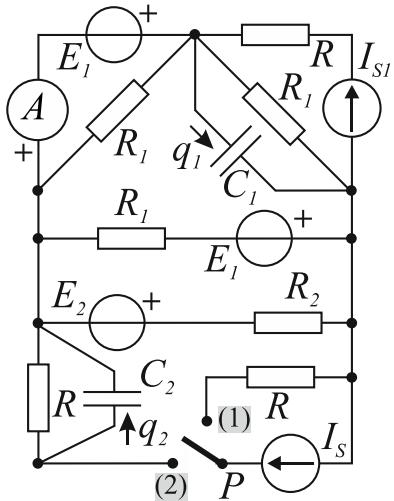
c)

$$U_{AB} = \int_A^B \vec{E} \cdot d\vec{l} = \int_a^b E dr = \int_a^c E_1 dr + \int_c^b E_2 dr = \int_a^c \frac{Q}{2\pi\epsilon_1 r L} dr + \int_c^b \frac{Q}{2\pi\epsilon_2 r L} dr = \frac{Q}{2\pi\epsilon_1 L} \ln \frac{c}{a} + \frac{Q}{2\pi\epsilon_2 L} \ln \frac{b}{c}$$

$$C = \frac{Q}{U_{AB}} \quad C = \frac{2\pi\epsilon_0 L}{\frac{1}{\epsilon_{r1}} \ln \frac{c}{a} + \frac{1}{\epsilon_{r2}} \ln \frac{b}{c}}$$

II-1

a)



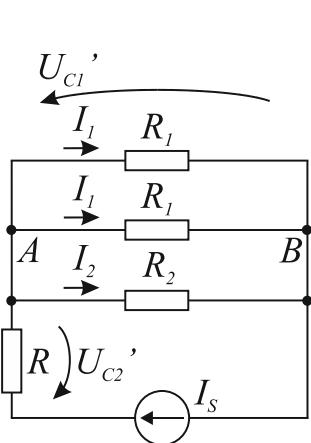
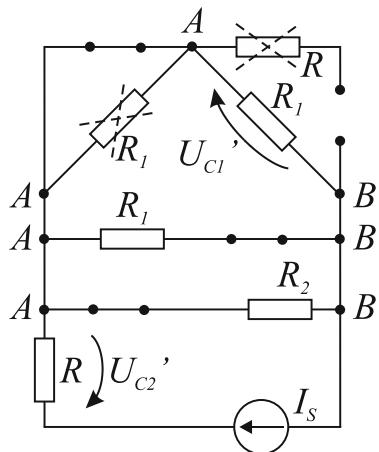
$$\begin{matrix} Svi \\ generatori \end{matrix} = \begin{matrix} Svi sem \\ I_s \end{matrix} + \begin{matrix} Samo \\ I_s \end{matrix}$$

(2) (1)

$$U_{C1}^{(2)} = U_{C1}^{(1)} + U_{C1}'$$

$$\Delta U_{C1} = U_{C1}^{(2)} - U_{C1}^{(1)} = U_{C1}'$$

$$U_{C1}' = \Delta U_{C1} = \frac{q_1}{C_1} = \frac{6 \text{ nC}}{4 \text{ nF}} = 1,5 \text{ V}$$



$$U_{AB} = U_{C1}' = 1,5 \text{ V}$$

$$I_1 = \frac{U_{AB}}{R_1} = \frac{1,5}{5} = 0,3 \text{ A}$$

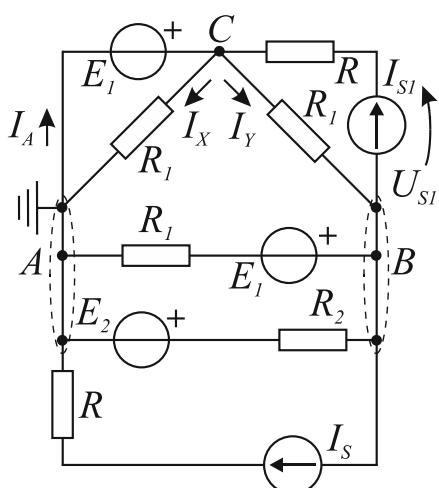
$$I_2 = \frac{U_{AB}}{R_2} = \frac{1,5}{10} = 0,15 \text{ A}$$

$$I_s = I_1 + I_2 \quad [I_s = 0,75 \text{ A}]$$

$$U_{C2}' = RI_s = 20 \cdot 0,75 = 15 \text{ V}$$

$$q_2 = C_2 U_{C2}' = 1 \cdot 10^{-9} \cdot 15 \quad [q_2 = 15 \text{ nC}]$$

b)



$$n_c = 3, \quad n_{i,n,g.} = 1$$

$$MP\check{C}: \quad n_c - 1 - n_{i,n,g.} = 3 - 1 - 1 = 1$$

$$V_A = 0 \text{ V}, \quad V_C = E_1 = 3 \text{ V}$$

$$\frac{V_B}{\infty} \left(\frac{1}{R_2} + \frac{1}{R_1} + \frac{1}{R_1} + \frac{1}{R_1} + \frac{1}{\infty} \right) - V_C \left(\frac{1}{R_1} + \frac{1}{\infty} \right) = -I_{S1} + \frac{E_2}{R_2} + \frac{E_1}{R_1} - I_{S1}$$

$$\frac{V_B}{10} \left(\frac{1}{5} + \frac{1}{5} + \frac{1}{5} \right) - 3 \cdot \left(\frac{1}{5} \right) = -0,75 + \frac{5}{10} + \frac{3}{5} - 0,5 \quad / \cdot 10$$

$$5V_B = 4,5 \quad \Rightarrow \quad V_B = 0,9 \text{ V}$$

$$U_{S1} = RI_{S1} + (V_C - V_B) = 20 \cdot 0,5 + (3 - 0,9) = 12,1 \text{ V}$$

$$P_{S1} = U_{S1} I_{S1} = 12,1 \cdot 0,5 \quad [P_{S1} = 6,05 \text{ W}]$$

c)

$$I_X = \frac{V_C - V_A}{R_1} = \frac{3 - 0}{5} = 0,6 \text{ A}$$

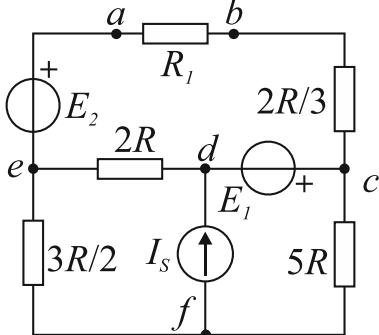
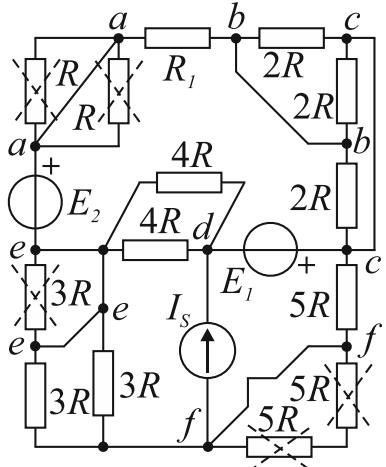
$$I_Y = \frac{V_C - V_B}{R_1} = \frac{3 - 0,9}{5} = 0,42 \text{ A}$$

$$I_A = I_X + I_Y - I_{S1} = 0,6 + 0,42 - 0,5$$

$$[I_A = 0,52 \text{ A}]$$

II-2

a)



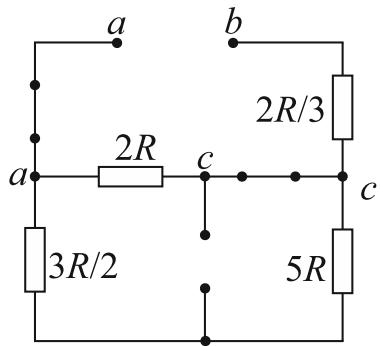
$$R_{bc} = 2R \parallel 2R \parallel 2R = \frac{2R}{3}$$

$$R_{cf} = 5R$$

$$R_{de} = 4R \parallel 4R = 2R$$

$$R_{ef} = 3R \parallel 3R = \frac{3R}{2}$$

b)

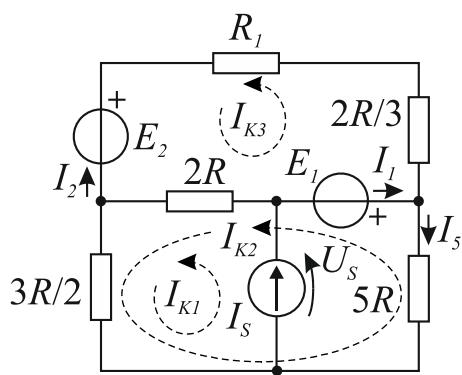


$$R_T = R_{ab} = \left[2R \parallel \left(\frac{3R}{2} + 5R \right) \right] + \frac{2R}{3} = \left(2R \parallel \frac{13R}{2} \right) + \frac{2R}{3}$$

$$R_T = \frac{26R}{17} + \frac{2R}{3} = \frac{78R}{51} + \frac{34R}{51} = \frac{112R}{51} = 112 \Omega$$

$$\boxed{R_l = R_T = 112 \Omega}$$

c)



$$n_g = 6, \quad n_c = 4, \quad n_{s.g.} = 1$$

$$MKS: \quad n_g - (n_c - 1) - n_{s.g.} = 6 - (4 - 1) - 1 = 3 - 1 = 2$$

$$K1: \quad I_{K1} = I_S = 1 A$$

$$K2: \quad \left(2R + 5R + \frac{3R}{2} \right) I_{K2} + \left(2R + \frac{3R}{2} \right) I_{K1} - 2R I_{K3} = -E_1$$

$$K3: \quad \left(R_1 + 2R + \frac{2R}{3} \right) I_{K3} - 2R I_{K1} - 2R I_{K2} = E_1 - E_2$$

$$K2: \quad \frac{17R}{2} I_{K2} + \frac{7R}{2} \cdot 1 - 2R I_{K3} = -51 \quad / \cdot \frac{2}{R}$$

$$K3: \quad \frac{248R}{51} I_{K3} - 2R \cdot 1 - 2R I_{K2} = 51 - 51 \quad / \cdot \frac{51}{R}$$

$$\left. \begin{aligned} 17I_{K2} - 4I_{K3} &= -9 \\ -102I_{K2} + 248I_{K3} &= 102 \end{aligned} \right\} \Rightarrow I_{K2} = -0,479 A, \quad I_{K3} = 0,214 A$$

$$P_{E1} = E_1 I_1 = E_1 (I_{K3} - I_{K2}) = 51 \cdot (0,214 + 0,479) = 51 \cdot 0,693 = 35,34 W$$

$$\boxed{P_{E1} = 35,34 W}$$

$$P_{E2} = E_2 I_2 = E_2 (-I_{K3}) = 51 \cdot (-0,214) = -10,91 W$$

$$\boxed{P_{E2} = -10,91 W}$$

$$U_s = -E_1 + 5R I_5 = -E_1 + 5R (-I_{K2}) = -51 + 5 \cdot 51 \cdot 0,479 = 71,15 V$$

$$P_s = U_s I_s = 71,15 \cdot 1 = 71,15 W$$

$$\boxed{P_s = 71,15 W}$$